



Technical Memorandum

Date: August 20, 2021

Project: Chehalis River Basin Flood Damage Reduction Project

To: Chehalis Basin Flood Control Zone District

From: HDR Andrew Little

Subject: Quarry Operations

Attachments: Attachment A. Figures
Attachment B. Quarry Boring Logs

1.0 Introduction and Purpose

The State Environmental Policy Act (SEPA) and National Environmental Policy Act (NEPA) Draft Environment Impact Statements (EIS) considered three potential quarry locations (North Quarry, South Quarry, and Huckleberry Ridge) to support construction of the proposed (Flood Retention Only - Expandable) FRE facility (Figure 1; all figures located in Attachment A). Since the release of the Draft EISs, the Chehalis Basin Flood Control Zone District (District) has determined that the Huckleberry Ridge location is not a viable option. To inform Final EIS development, this technical memorandum (TM) advances the concept of the viable quarry sites and further refines the assumptions for site location and extent of quarry development and operations during construction of the FRE facility. The previous work completed by HDR and Shannon & Wilson is the basis for this TM which advances the technical quantities of the quarries. Relevant boring logs are provided in Attachment B.

The FRE facility would require development of about 890,000 cubic yards (CY) or 1.7 million tons of aggregate materials (based on a bulking factor of 1.25 resulting from laboratory testing of the basalt that shows a density of 162 pounds per cubic foot [pcf] and assuming in place bulk density of 130 pcf). The amount of material required for road base and riprap have not been defined in detail. However, a quarry capable of generating up to 2 times the aggregate required for the FRE facility is expected to provide a sufficient margin of safety required to the combined aggregate, road base, and riprap with a suitable allowance for waste associated with unacceptable rock such as weathered basalt or interbedded siltstone materials. It is unlikely the quarry rock would be suitable for conventional concrete and material would need to be furnished from off-site.

1.1 Quarry Descriptions

Potential quarry sites for obtaining construction materials for the proposed flood retention structure (aggregate for roller compacted concrete [RCC], road base and riprap) were first identified through a regional geologic mapping and assessment process. Following identification of a candidate quarry site, a sequence of site investigations, laboratory testing, and engineering assessments were performed.

The following quarry descriptions provide the quarry locations and a summary of the field investigations that have been completed including geotechnical borings and seismic refraction survey lines. For site investigation methodology details and results refer to the Phase 2 Site Characterization TM (HDR 2017) and the Phase 3 Geotechnical Data Report (Shannon & Wilson, Inc. 2019).

North Quarry: The North Quarry is located about 1.2 miles directly southeast (2.14 miles by road) of the proposed FRE facility site and within the limits of the detention pool. The site is accessed off the main Road 1000 by Road 1013 (Figure 1). One seismic refraction survey line and four borings (one in 2016 and three in 2018) have been completed at this potential quarry site (Figure 2).

South Quarry: The South Quarry is located about 2.5 miles directly south (4.3 miles by road) of the proposed FRE facility site and also within the limits of the detention pool. The site is accessed off the main Road 1000 by the Road 1020 southwest of the site as it rises to the northeast and exposes a basalt outcrop along the southeastern margin of the site (Figure 1). This quarry site was added following the Phase 2 investigation when a Weyerhaeuser contractor improved the grade of the 1020 Road, west of the mainstem Chehalis River, exposing basalt not previously visible. A grab sample of the rock from that road cut was tested in early 2018 and tests indicated that the rock may be promising for use as aggregate. Consequently, a boring was included in the Phase 3 investigation (Figure 3), but no seismic refraction survey has been performed.

2.0 Quarry Quantity Estimates

Limited investigations have been performed at both quarry sites. Hence, significant uncertainties remain regarding depth of overburden, thickness of quality rock, and the lateral extents that would be required. Further drilling investigations would be required to develop a final quarry plan. Therefore, the quantity estimates described in the following sections should only be considered a rough order of magnitude and subject to future verification.

2.1 North Quarry

Figure 2 shows the proposed extents of the North Quarry and the locations of the four borings and one seismic refraction survey line conducted to assess the quality and quantity of basalt to be used as aggregate, road base, and riprap. The area of the potential quarry is estimated at 820,000 square feet (sf) or 18.8 acres (ac). Table 1 shows the estimated overburden and basalt bedrock thicknesses from each of the four borings and the potential total volume of overburden waste and processed rock that could be produced using the estimated quarry area.



Table 1. North Quarry Boring Result Summary

| Boring ID | Thickness (ft) | |
|---------------------|------------------|------------------|
| | Overburden | Basalt |
| RNQ-16-301 (QB1) | 38 | 76 |
| RNQ-18-301 | 75 | 45 |
| RNQ-18-302 | 48 | 30 |
| RNQ-18-303 | 45 | 55 |
| Average: | 51.5 | 51.5 |
| Volume (CY): | 1,564,074 | 1,564,074 |

By averaging the thickness for both overburden and basalt between the four borings, the volume of each is about 1.5 million CY. The boring logs indicate only a few siltstone interbeds on the order of 6 inches thick. This would result in a minimal amount of waste material (expected to be less than 10%) within the basalt resulting in about 1.4 million CY or about 3.1 million tons of usable rock. The necessary volume of aggregate is about 890,000 CY for the RCC dam (HDR 2018), or about 1.7 million tons resulting in a calculated factor of safety of 1.8. Some of this excess material would be used for road base and riprap but quantities for these are not well defined and can be assumed to be included in the factor of safety.

It should be noted that the seismic refraction survey was not consistent with the boring data and displayed an overburden thickness ranging from 70 to 90 feet. Also, below the basalt is a layer of siltstone that is the lower boundary of useable bedrock. If the overburden thickness is greater than what is shown in the boring logs, as indicated by the seismic refraction survey, then the lateral extents of the quarry area may need to be increased to mine sufficient quantities of basalt for all the aggregate, road base, and riprap that may be required for the project.

2.2 South Quarry

The proposed extents of the South Quarry are shown on Figure 3 as well as the location of the boring conducted to assess the quality and quantity of basalt for use as aggregate, road base, and riprap. The area of the potential quarry is estimated at 750,000 sf or 17.2 ac. Table 2 summarizes the boring log stratigraphy.



Table 2. South Quarry Boring Result Summary

| Depth (ft) | | Thickness (ft) | Description |
|------------|-----|----------------|-------------------|
| From | To | | |
| 0 | 35 | 35 | Overburden |
| 35 | 133 | 98 | Basalt |
| 133 | 146 | 13 | Breccia/siltstone |
| 146 | 180 | 34 | Basalt |

Notes:

Total basalt thickness: 132 feet

The boring ended at 180 feet within basalt which may extend beyond the depth of the boring.

The single boring in the potential quarry indicates an overburden thickness of 35 feet which results in an estimated useable rock volume of about 980,000 CY. Within the potentially usable basalt bedrock, there is a layer of basalt breccia and siltstone that would be wasted resulting in a total thickness of usable basalt of 132 feet. The boring log indicates several zones of weak and highly weathered rock within the usable basalt, which is more variability than seen in the basalt at the North Quarry. A 30 percent waste factor was applied to be conservative. When a thickness of 132 feet is multiplied by the quarry area (750,000 sf) and reduced by the 30 percent waste factor, the resulting volume is about 2.6 million CY or about 6 million tons. This provides a factor of safety of 3.4, using the required tonnage (1.7 million tons). With only a single boring, there is significant uncertainty to the calculated quantities and thus a much higher factor of safety is appropriate for the South Quarry.

2.3 Quarry Quantity Summary

The quantities for each quarry are summarized based on the limited amount of existing data in Table 3. Further investigation and analysis is required to verify these values.

Table 3. Summary of Quarry Quantities

| Item | Unit | North Quarry | South Quarry |
|------------------------------------|------|--------------|--------------|
| Area | sf | 819,760 | 755,714 |
| Overburden Volume ¹ | CY | 1,564,074 | 978,704 |
| Overburden Weight ² | tons | 2,639,375 | 1,651,563 |
| Initial Basalt Volume | CY | 1,564,074 | 3,691,111 |
| Waste Factor | CY | 10% | 30% |
| Expected Waste Volume ¹ | CY | 156,407 | 1,107,333 |
| Useable Basalt Volume | CY | 1,407,667 | 2,583,778 |



| Item | Unit | North Quarry | South Quarry |
|------------------------------------|------|--------------|--------------|
| Useable Basalt Weight ³ | tons | 3,078,568 | 5,650,722 |
| Factor of Safety ⁴ | -- | 1.8 | 3.4 |

Notes:

1. No bulking factor was applied to the overburden volume.
2. A bulk density of 125 pcf was assumed for overburden.
3. Laboratory testing indicates a density of 162 pcf for the basalt.
4. Factor of Safety based on a need of 890,000 CY (HDR 2018) or 1,685,880 tons using a bulking factor of 1.25 based on laboratory results of the basalt and assuming an in-place density of 130 pcf.

3.0 Quarry Equipment and Operational Time

Quarry and aggregate processing assumptions reflect equipment and construction approaches typical of large-quantity, project-dedicated, stripping, quarrying, and quarried-rock aggregate processing. A wide variety of equipment and production approaches could be employed which the following assumptions should reasonably represent.

3.1 North Quarry

Overburden excavation equipment would involve large dozers (100,000 to 200,000 pounds, 350- to 550-horsepower [hp]), large excavators (100,000 to 230,000 pounds, 450- to 550-hp), and 35- to 45-ton (400- to 500-hp) articulated off-road haul trucks and/or 50- to 70-ton (500- to 800-hp) off-road haul trucks. Overburden excavation operations could be expected to take 8–12 months.

Similar equipment should be expected for the quarry drilling, blasting, and excavation for crusher feed; but including rock drills (400 hp +/-).

Crushing and processing equipment is likely to include large jaw primary crushing, cone, or vertical shaft impact secondary crushing, and vertical shaft impact tertiary crushing; together with associated feeders, conveyors, screen decks, and potentially aggregate washing equipment. Aggregate processing operations could be expected to utilize 1,000 to 2,000 operating horsepower over a period of 12 to 20 months.

3.2 South Quarry

South quarry operations would look similar to the north quarry operations but be expected to involve approximately half of the time for overburden excavation.

4.0 Summary

This memo clarifies the viability of the two proposed quarry sites, north and south quarry for supplying aggregate for the construction of the proposed FRE facility. This information is intended to refine the assumptions regarding the operations at either of these sites for development of the Final EISs. Additionally, each individual quarry site may supply sufficient material for construction of the proposed project. As the contractor develops the quarry, they may be able to utilize a single quarry or a portion of both quarries depending on quality and

quantity of rock, however further investigations will be required to determine if one or both quarries will be utilized.

5.0 Literature Cited

HDR Engineering, Inc. (HDR)

- 2017 Phase 2 Site Characterization Technical Memorandum.
- 2018 Combined Dam and Fish Passage Supplemental Design Report FRE Dam Alternative.

Shannon & Wilson (S&W)

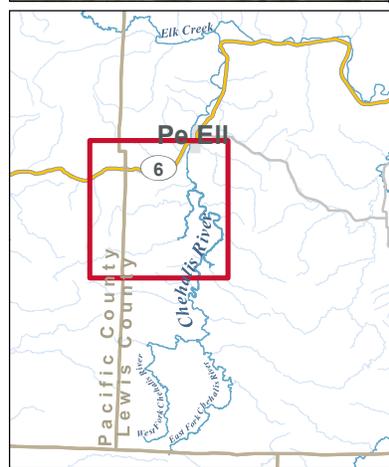
- 2019 Phase 3 Chehalis Dam Geotechnical Data Report, Chehalis Basin Work Group, Pe EII, Washington.

Attachment A. Figures

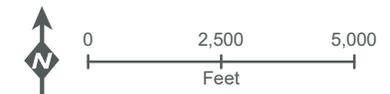
Figure 1. Potential Quarry Sites under Consideration

Figure 2. North Quarry Site Plan

Figure 3. South Quarry Site plan



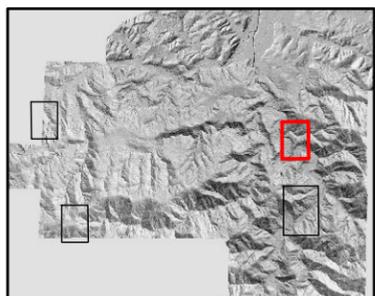
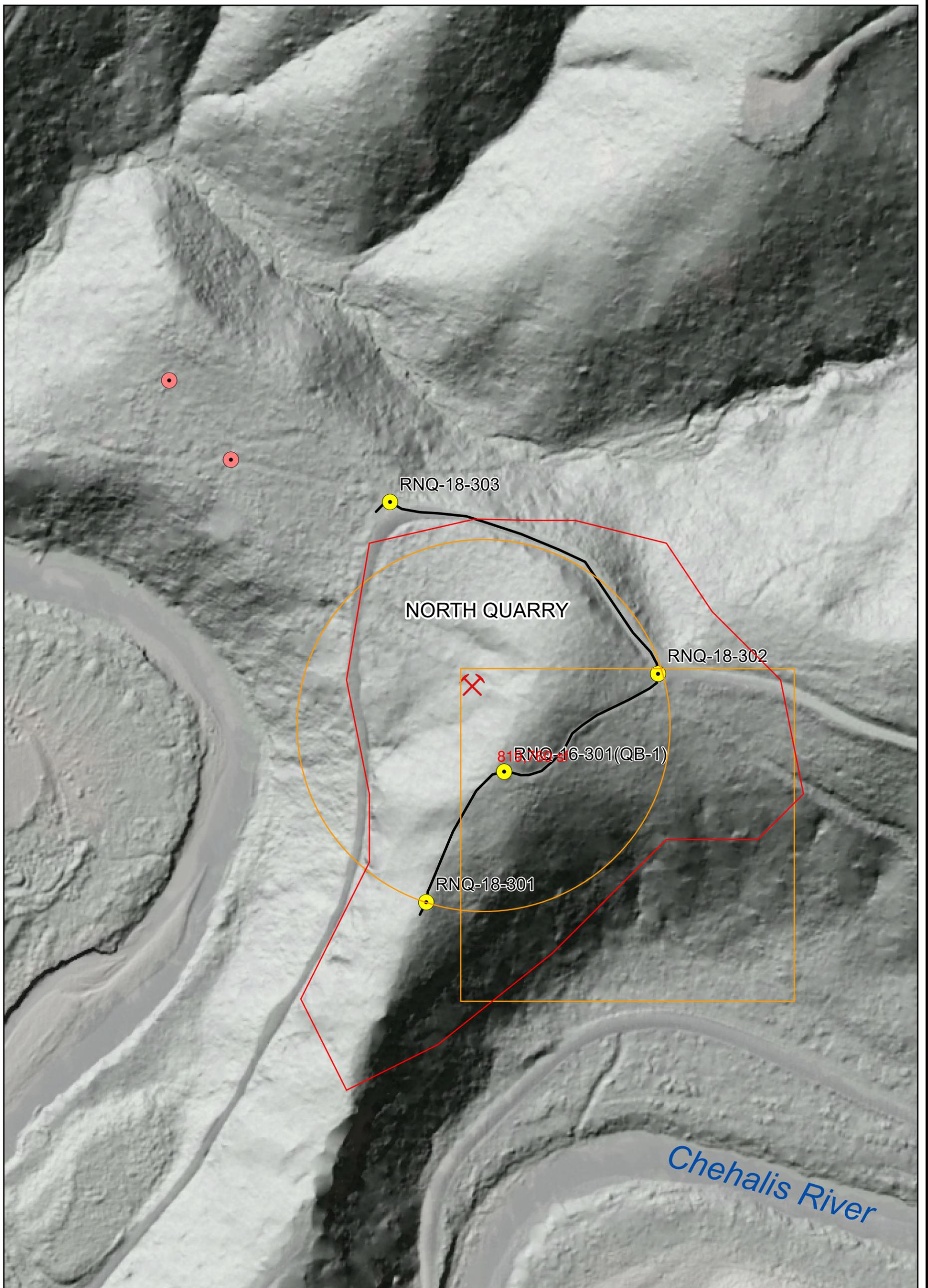
- Quarry Site
- Concrete Production Facility
- Existing roads to be improved for quarry site access
- Main channel OHWM



NAD 1983 STATE PLANE WASHINGTON SOUTH FT (FIPS 4602)

FIGURE 1
POTENTIAL QUARRY SITES UNDER CONSIDERATION

CHEHALIS RIVER BASIN FLOOD DAMAGE REDUCTION PROJECT



LEGEND

- Landslide Location and Designation
 LS-26
- Quarry Site Location
- Profile Location
- Potential Dam Site Location
- Completed Boring Locations
- Recommended Boring Locations

NOTE:
 Hillshade generated using ESRI 3D Analyst from LIDAR data provided by HDR. NAVD 88, Illumination 315

0 300
 Feet

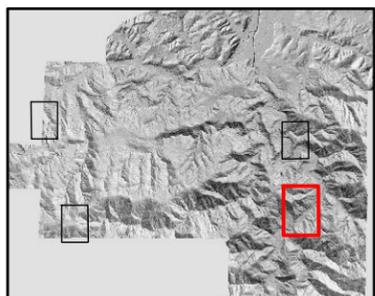
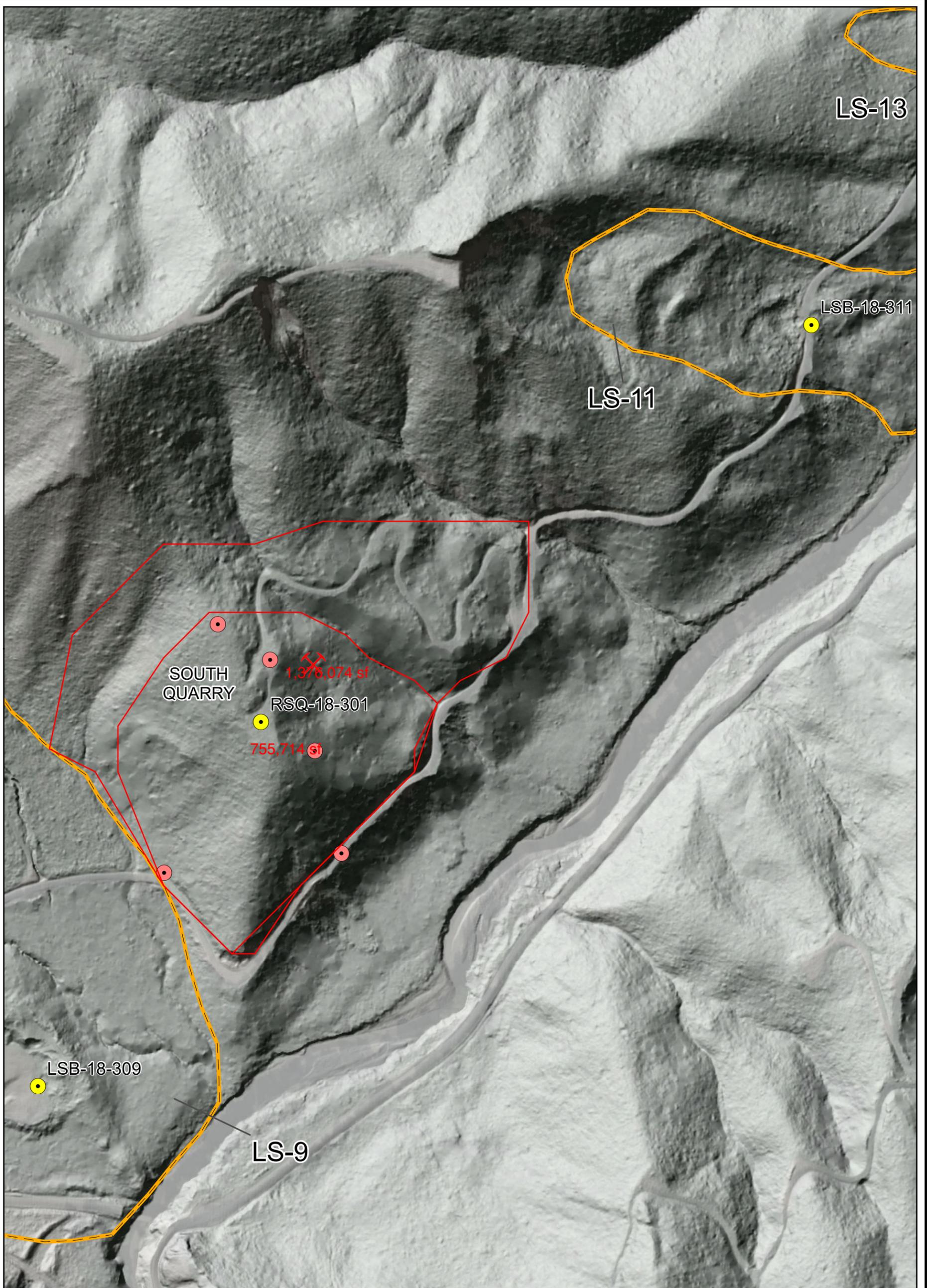
Chehalis Dam
 Rock Quarry Characterization
 Pe Ell, Washington

SITE PLAN

March 2019 21-1-21897-025

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 GEOTECHNICAL AND ENVIRONMENTAL CONSULTANTS

FIG. 2
 Page 1 of 4



LEGEND

- Landslide Location and Designation
 LS-26
- Quarry Site Location
- Profile Location
- Potential Dam Site Location
- Completed Boring Locations
- Recommended Boring Locations

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0 300
 Feet

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 Rock Quarry Characterization
 Pe Ell, Washington

SITE PLAN

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SHANNON & WILSON, INC.
 GEOTECHNICAL AND ENVIRONMENTAL CONSULTANTS

FIG. 2
 Page 2 of 4



Attachment B. Quarry Boring Logs

| Groundwater Measurements | | |
|--------------------------|------|------------|
| Date | Time | Depth (ft) |
| | | |
| | | |
| | | |

Chehalis Dam Site Characterization



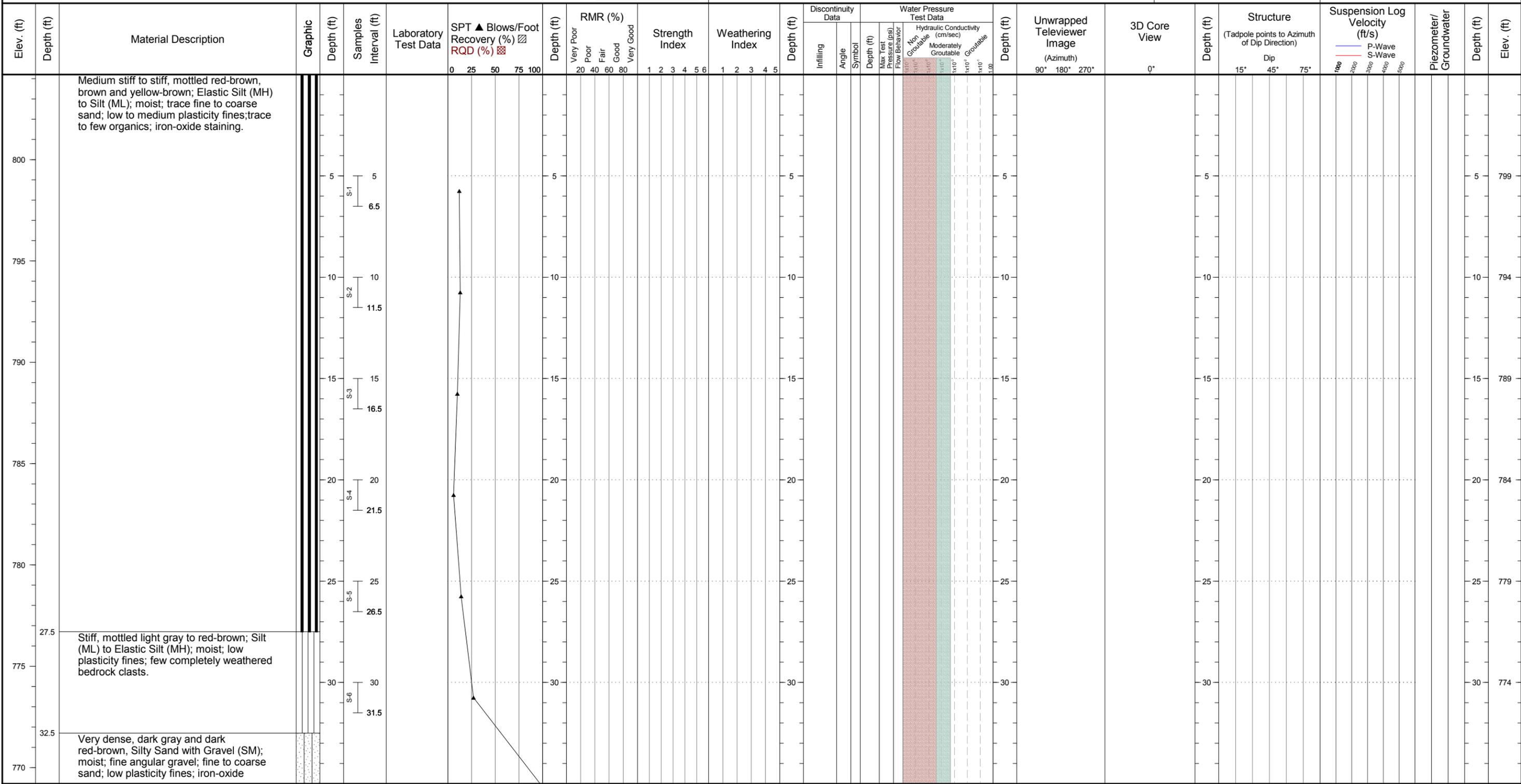
QB-1

Sheet 1 of 5

Client: Anchor QEA

Phase 2

Project No: 268421



| LITHOLOGY KEY | | |
|---------------|---------|-----------|
| | MH | CLAYSTONE |
| | ML | BASALT |
| | SM | SILTSTONE |
| | BRECCIA | |

| SAMPLES | |
|---------|-------------|
| # | TYPE |
| 1 | SPT Sample |
| 2 | Tube Sample |
| 3 | Core Run |

| TEST DATA | |
|-----------|---|
| ● | Moisture Content (%) |
| ○ | Fines (<0.075mm) (%) |
| LL | Liquid Limit |
| PL | Plastic Limit |
| DD | Dry Density (pcf) |
| X | Slake Durability Test (Index% - type descriptions to the right) |
| BD | Bulk Density (pcf) |
| * | Unconfined Compressive Strength (psi) |
| ⊙ | Point Load Test (psi) |
| SG | Specific Gravity |
| n | Porosity |
| φ | Peak Friction Angle (degrees) |
| c | Peak Cohesion (psi) |
| abs | Absorption (%) |
| ASR | Alkali Silica Reactivity (16 day avg. % length change) |
| LA | LA Abrasion (% loss) |

| SLAKE DURABILITY TEST | |
|-----------------------|---|
| TYPE | Description |
| I | Retained specimen remains virtually unchanged |
| II | Retained specimen consists of large and small fragments |
| III | Retained specimen is exclusively small fragments |

| STRENGTH INDEX | | |
|------------------|-------|--------------------------|
| TERM | INDEX | APPROX. UCS (psi x 1000) |
| Very Weak | 1 | <0.7 |
| Weak | 2 | 0.7 to 3.6 |
| Medium Strong | 3 | 3.6 to 7.2 |
| Strong | 4 | 7.2 to 14.5 |
| Very Strong | 5 | 14.5 to 36.25 |
| Extremely Strong | 6 | >36.25 |

| WEATHERING INDEX | | |
|------------------|-------|--|
| TERM | INDEX | DESCRIPTION |
| Fresh | 1 | No evidence of alteration |
| Slightly | 2 | Slight discoloration on surface |
| Moderately | 3 | Discoloring evident, alteration well below rock surfaces |
| Highly | 4 | Entire mass discolored |
| Completely | 5 | Rock reduced to a soil with relict rock texture |

| DISCONTINUITY DATA | |
|--------------------|---|
| INFILLING | ANGLE |
| CA: Calcite | Degrees relative to horizontal plane, (-) below plane |
| CL: Clay | |
| FE: Iron Oxide | |
| M: Mineral | |
| S: Sand | |
| G: Gouge | |
| SS: Slickensides | |
| H: Healed | |
| SYMBOL | |
| | Fracture |
| | Healed |
| | Rubble Zone |
| | Gouge Zone |
| | Core Loss |

| PIEZOMETER | |
|------------|-----------------------------------|
| | Vibrating Wire Piezometer |
| | Surface Cement Seal |
| | Bentonite Cement Grout |
| | Bentonite Seal |
| | Sand Filter |
| | Slough |
| | Groundwater Level During Drilling |
| | Groundwater Level and Date Read |

| STRUCTURE | |
|-----------|-------------------------------|
| | Major open joint/fracture |
| | Minor open joint/fracture |
| | Partially open joint/fracture |
| | Filled joint/fracture |
| | Bedding/Banding/Foliation |
| | Contact |

DEFINITIONS
 1. USCS: Unified Soil Classification System; Standard Practice for Classification of Soils for Engineering Purposes - ASTM D2487
 2. SPT: Standard Penetration Test; Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils - ASTM D1586
 3. RQD: Rock Quality Designation; Standard Test Method for Determining Rock Quality Designation (RQD) of Rock Core - ASTM D6932
 4. RMR: Rock Mass Rating; The Rock Mass Rating (RMR) System (Geomechanics Classification) in Engineering Practice - STP984 (see references)

NOTES
 1. The contacts represent the approximate boundaries between lithology types, and the transition may be gradual.
 2. The discussion in the text of this report is necessary for a proper understanding of the nature of the subsurface materials.
 3. The location of the discontinuities shown are approximate. For clarity not all discontinuities are shown.
 4. Grab samples taken from the core for laboratory testing

REFERENCES
 1. Discontinuity, weathering, strength and roughness terms used in Material Descriptions are from (Brown, E.T., Editor, 1981, Rock Characterization Testing and Monitoring, ISRM Suggested Methods, pp. 5, 31, 32.)
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 3. RMR values are derived using the method from (Bieniawski, Z.T., 1989, Engineering rock mass classifications, New York: Wiley)

| Groundwater Measurements | | |
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| Date | Time | Depth (ft) |
| | | |
| | | |
| | | |

Chehalis Dam Site Characterization



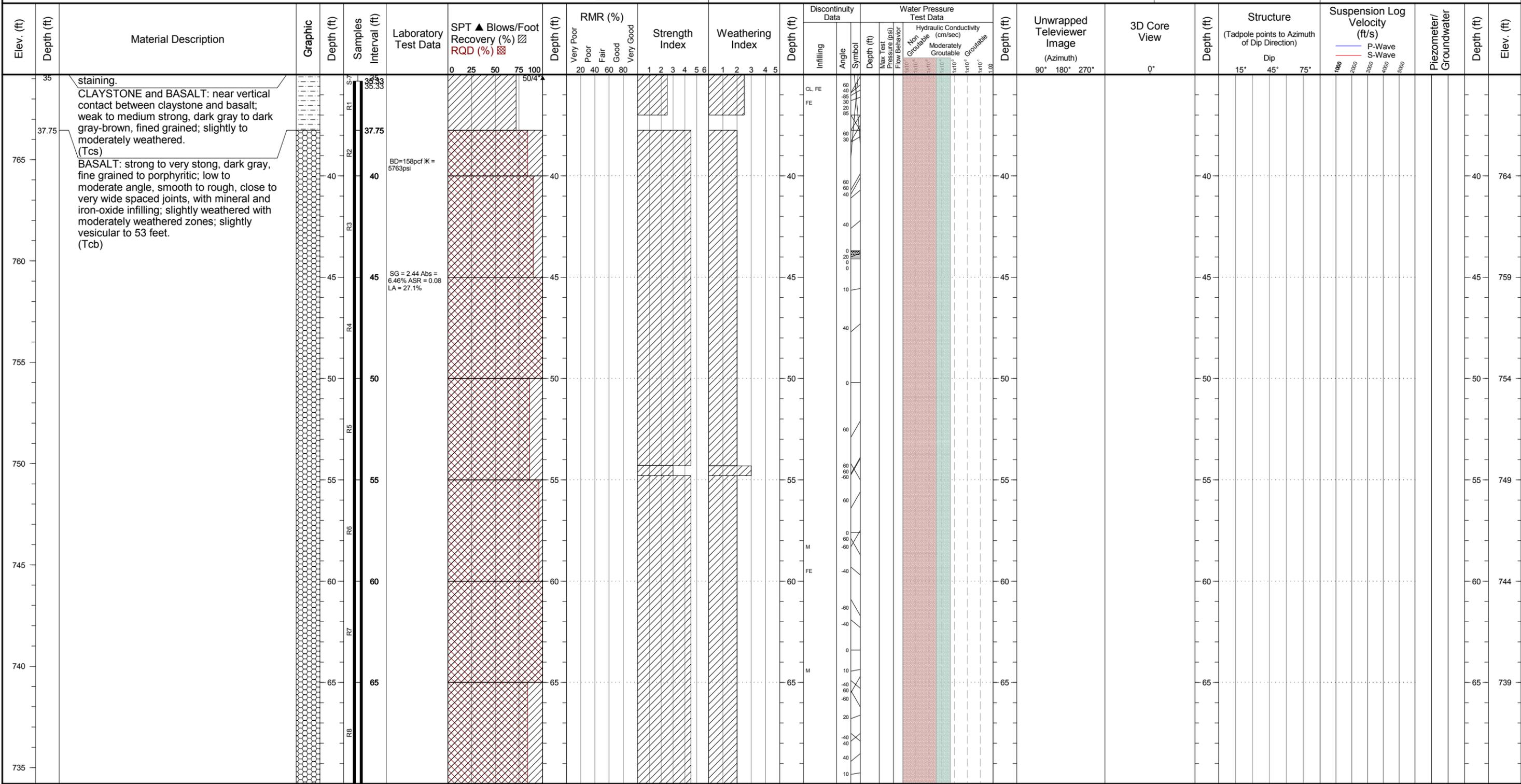
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Sheet 2 of 5

Client: Anchor QEA

Phase 2

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| SAMPLES | |
|---------|-------------|
| # | TYPE |
| ○ | SPT Sample |
| □ | Tube Sample |
| ■ | Core Run |

| TEST DATA | |
|-----------|---|
| ● | Moisture Content (%) |
| ○ | Fines (<0.075mm) (%) |
| LL | Liquid Limit |
| PL | Plastic Limit |
| DD | Dry Density (pcf) |
| X | Slake Durability Test (Index% - type descriptions to the right) |
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| * | Unconfined Compressive Strength (psi) |
| ⊛ | Point Load Test (psi) |
| SG | Specific Gravity |
| n | Porosity |
| φ | Peak Friction Angle (degrees) |
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| ASR | Alkali Silica Reactivity (16 day avg. % length change) |
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| H: Healed | |

| PIEZOMETER | |
|------------|-----------------------------------|
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| □ | Surface Cement Seal |
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Chehalis Dam Site Characterization

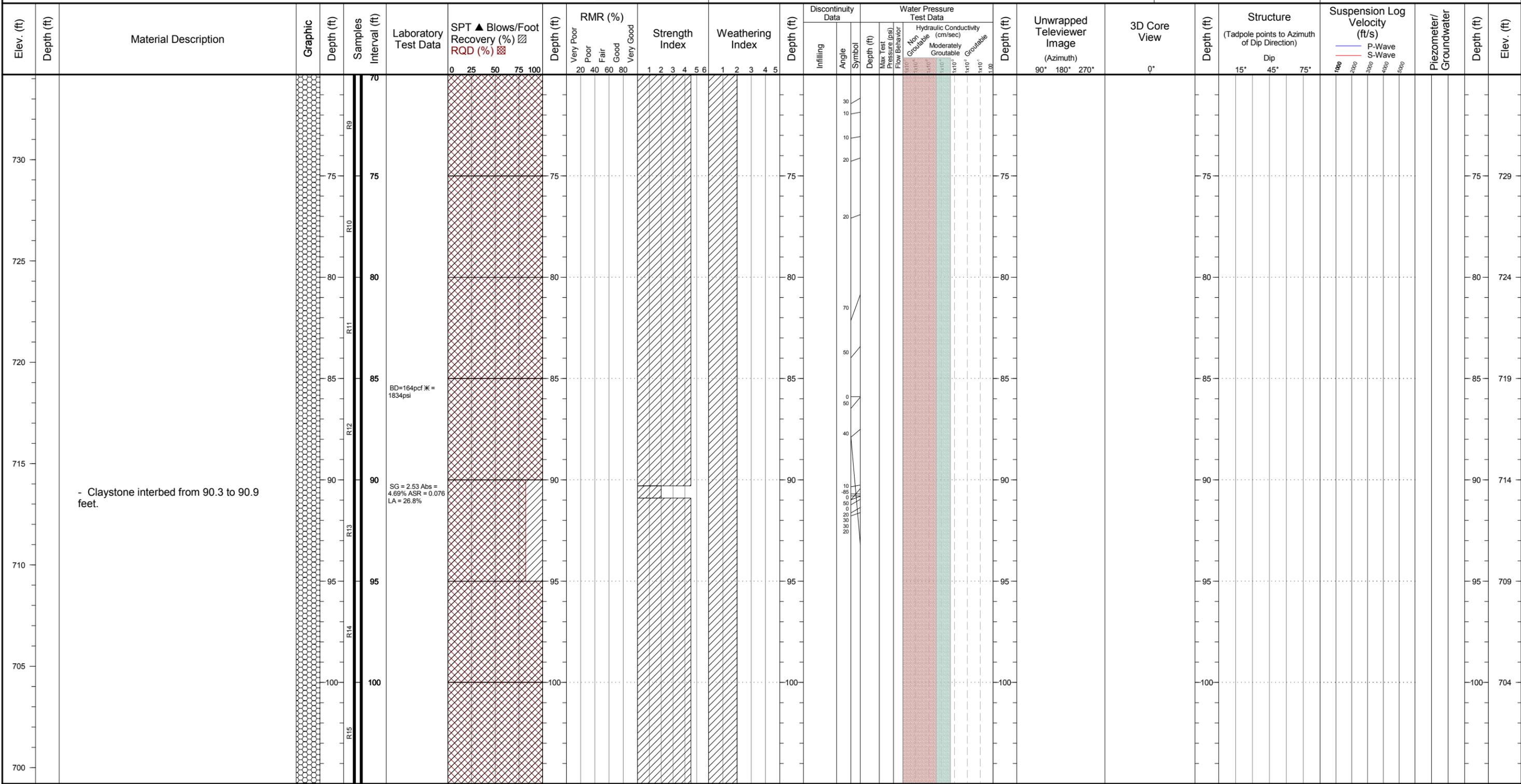


QB-1
Sheet 3 of 5

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Phase 2

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| H: Healed | |
| SYMBOL | |
| ▬ | Fracture |
| ▬ | Healed |
| ▬ | Rubble Zone |
| ▬ | Gouge Zone |
| ▬ | Core Loss |

| PIEZOMETER | |
|------------|-----------------------------------|
| ▬ | Vibrating Wire Piezometer |
| ▬ | Surface Cement Seal |
| ▬ | Bentonite Cement Grout |
| ▬ | Bentonite Seal |
| ▬ | Sand Filter |
| ▬ | Slough |
| ▬ | Groundwater Level During Drilling |
| ▬ | Groundwater Level and Date Read |

| STRUCTURE | |
|-----------|-------------------------------|
| ▬ | Major open joint/fracture |
| ▬ | Minor open joint/fracture |
| ▬ | Partially open joint/fracture |
| ▬ | Filled joint/fracture |
| ▬ | Bedding/Banding/Foliation |
| ▬ | Contact |

DEFINITIONS
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| Groundwater Measurements | | |
|--------------------------|------|------------|
| Date | Time | Depth (ft) |
| | | |
| | | |
| | | |

Chehalis Dam Site Characterization



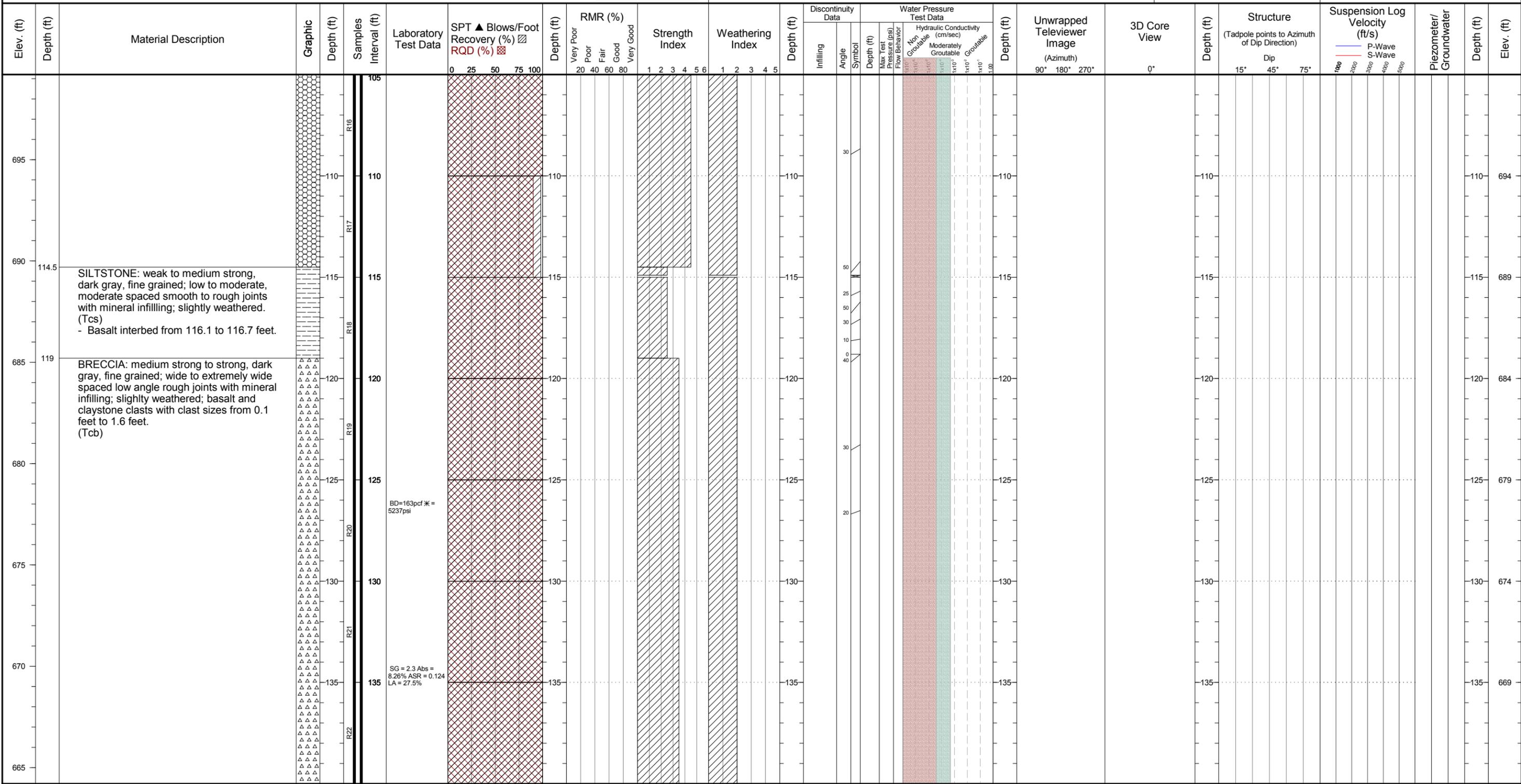
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Client: Anchor QEA

Phase 2

Project No: 268421



| LITHOLOGY KEY | | |
|---------------|-----------|---------|
| MH | CLAYSTONE | BRECCIA |
| ML | BASALT | |
| SM | SILTSTONE | |

| SAMPLES | |
|---------|-------------|
| # | TYPE |
| ○ | SPT Sample |
| ○ | Tube Sample |
| ○ | Core Run |

| TEST DATA | |
|-----------|--|
| ● | Moisture Content (%) |
| ○ | Fines (<0.075mm) (%) |
| LL | Liquid Limit |
| PL | Plastic Limit |
| DD | Dry Density (pcf) |
| X | Slake Durability Test (Index) - type descriptions to the right |
| BD | Bulk Density (pcf) |
| * | Unconfined Compressive Strength (psi) |
| ⊛ | Point Load Test (psi) |
| SG | Specific Gravity |
| n | Porosity |
| α | Peak Friction Angle (degrees) |
| c | Peak Cohesion (psi) |
| abs | Absorption (%) |
| ASR | Alkali Silica Reactivity (16 day avg. % length change) |
| LA | LA Abrasion (% loss) |

| SLAKE DURABILITY TEST | |
|-----------------------|---|
| TYPE | Description |
| I | Retained specimen remains virtually unchanged |
| II | Retained specimen consists of large and small fragments |
| III | Retained specimen is exclusively small fragments |

| STRENGTH INDEX | | |
|------------------|-------|--------------------------|
| TERM | INDEX | APPROX. UCS (psi x 1000) |
| Very Weak | 1 | <0.7 |
| Weak | 2 | 0.7 to 3.6 |
| Medium Strong | 3 | 3.6 to 7.2 |
| Strong | 4 | 7.2 to 14.5 |
| Very Strong | 5 | 14.5 to 36.25 |
| Extremely Strong | 6 | >36.25 |

| WEATHERING INDEX | | |
|------------------|-------|--|
| TERM | INDEX | DESCRIPTION |
| Fresh | 1 | No evidence of alteration |
| Slightly | 2 | Slight discoloration on surface |
| Moderately | 3 | Discoloring evident, alteration well below rock surfaces |
| Highly | 4 | Entire mass discolored |
| Completely | 5 | Rock reduced to a soil with relict rock texture |

| DISCONTINUITY DATA | |
|--------------------|---|
| IN FILLING | ANGLE |
| CA: Calcite | Degrees relative to horizontal plane, (-) below plane |
| CL: Clay | |
| FE: Iron Oxide | |
| M: Mineral | |
| S: Sand | |
| G: Gouge | |
| SS: Slickensides | |
| H: Healed | |

| PIEZOMETER | |
|------------|-----------------------------------|
| ○ | Vibrating Wire Piezometer |
| ○ | Surface Cement Seal |
| ○ | Bentonite Cement Grout |
| ○ | Bentonite Seal |
| ○ | Sand Filter |
| ○ | Slough |
| ○ | Groundwater Level During Drilling |
| ○ | Groundwater Level and Date Read |

| STRUCTURE | |
|-----------|-------------------------------|
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| | | |
| | | |
| | | |

Chehalis Dam Site Characterization

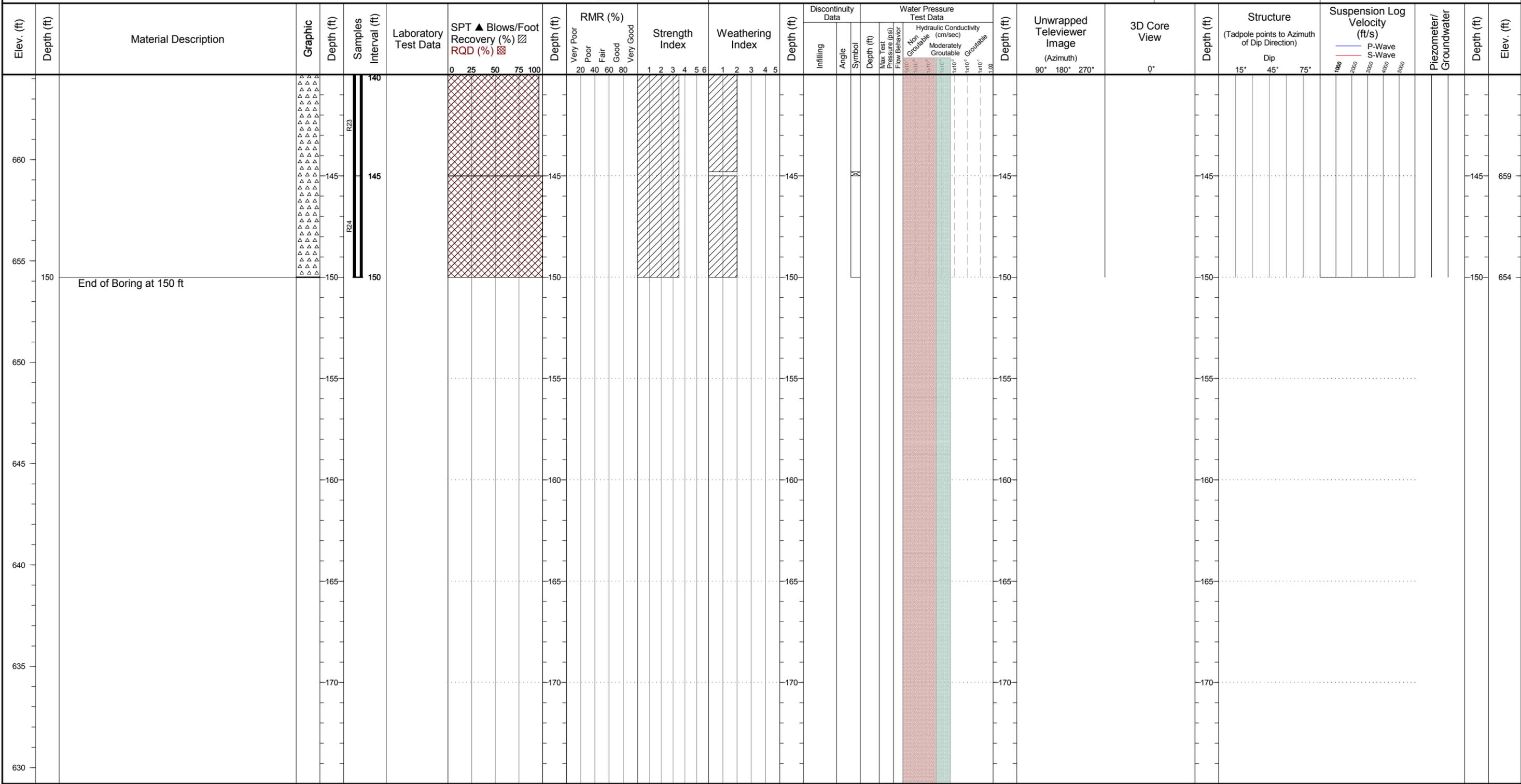


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Sheet 5 of 5

Client: Anchor QEA

Phase 2

Project No: 268421



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| G: Gouge | |
| SS: Stickensides | |
| H: Healed | |
| SYMBOL | |
| Fracture | |
| Healed | |
| Rubble Zone | |
| Gouge Zone | |
| Core Loss | |

| PIEZOMETER | |
|------------|-----------------------------------|
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